

# ASCENT – Performance criteria and benchmarking (WP1)

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EU – Australia workshop

Lausanne, 14<sup>th</sup> November 2016



## Scope of the activity

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To perform process integration study and techno-economic analysis of Ascent technologies in full scale power plants and hydrogen plants and compare with benchmark technologies.

# Summary of the presentation

- ❖ **Benchmark power plants and hydrogen plants**
- ❖ **Process integration and simulation of Ascent technologies:**
  - SER process in SOFC-based power plant
  - SER process in combined cycle power plant
  - Ca/Cu process in combined cycle power plant
  - C-Shift process in combined cycle power plant
- ❖ **Preliminary economic evaluation of power plants:**
- ❖ **Conclusions and next activities**

# Benchmark power plants and hydrogen plants

Benchmark plants for power and hydrogen production:

No Capture

CO<sub>2</sub> Capture

Combined cycle power plants:

1. **NGCC** (Natural Gas Combined Cycle) - *EBTF*
2. **NGCC+MEA** (NGCC with post-combustion capture by MEA) - *EBTF*
3. **ATR+MDEA** (Autothermal reformer+pre-combustion capture)

Coal power plants:

4. **IGCC** (Integrated Gasification Combined Cycle) - *EBTF*
5. **IGCC+Selexol** (IGCC with pre-combustion capture by Selexol) - *EBTF*

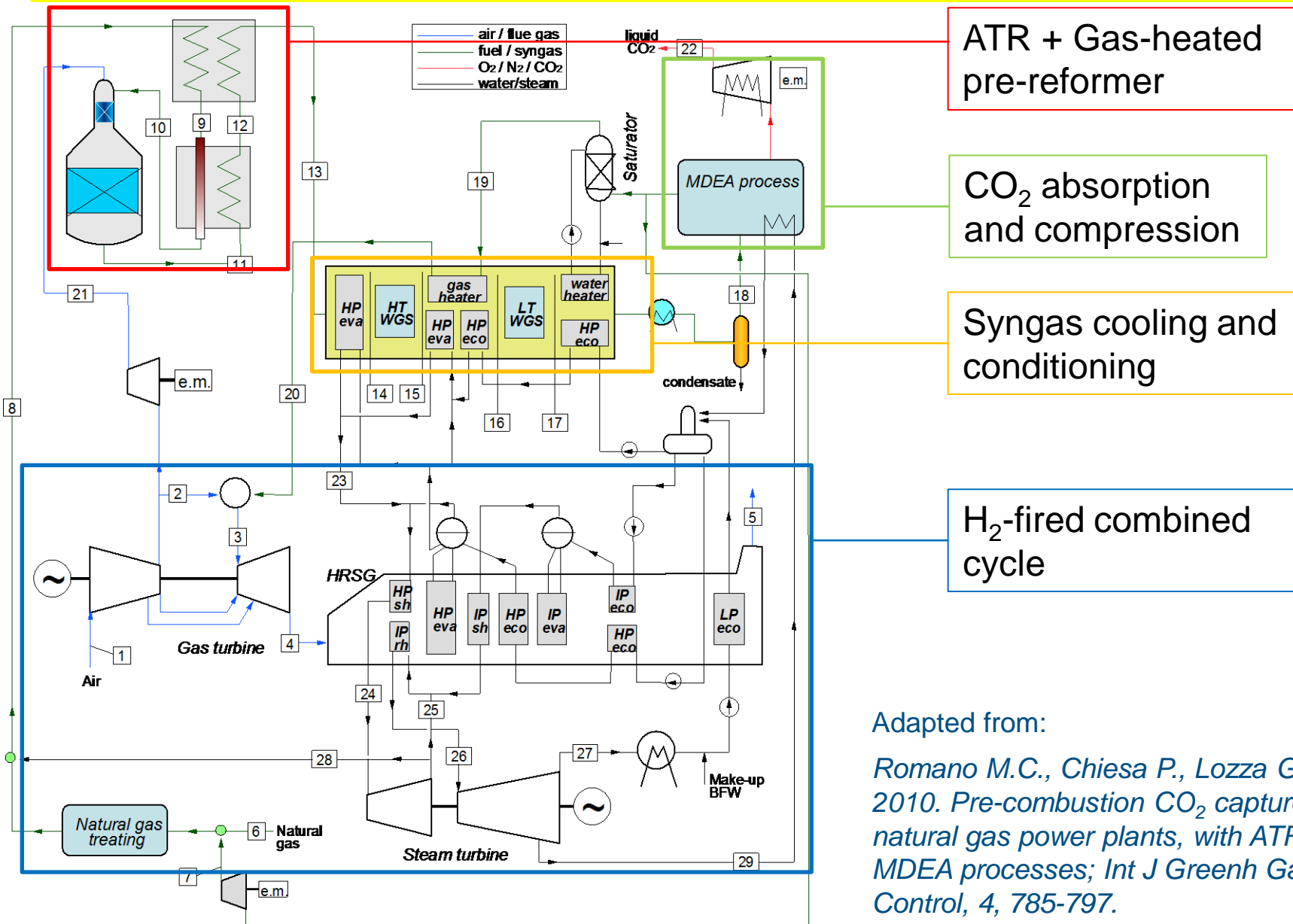
SOFC power plants:

6. **ATM w/o CCS** (Atmospheric SOFC without capture)
7. **ATM with CCS** (With cryogenic CO<sub>2</sub> separation)
8. **PRESS w/o CCS** (Pressurized SOFC without capture)
9. **PRESS with CCS** (With cryogenic CO<sub>2</sub> separation)

H<sub>2</sub> production plants:

10. **FTR** (Fired Tubular Reformer)
11. **FTR+MDEA** (FTR with CO<sub>2</sub> medium capture by MDEA)
12. **FTR+MDEA** (FTR with CO<sub>2</sub> high capture by MDEA)

# Benchmark power plants – ATR+MDEA



ATR + Gas-heated pre-reformer

CO<sub>2</sub> absorption and compression

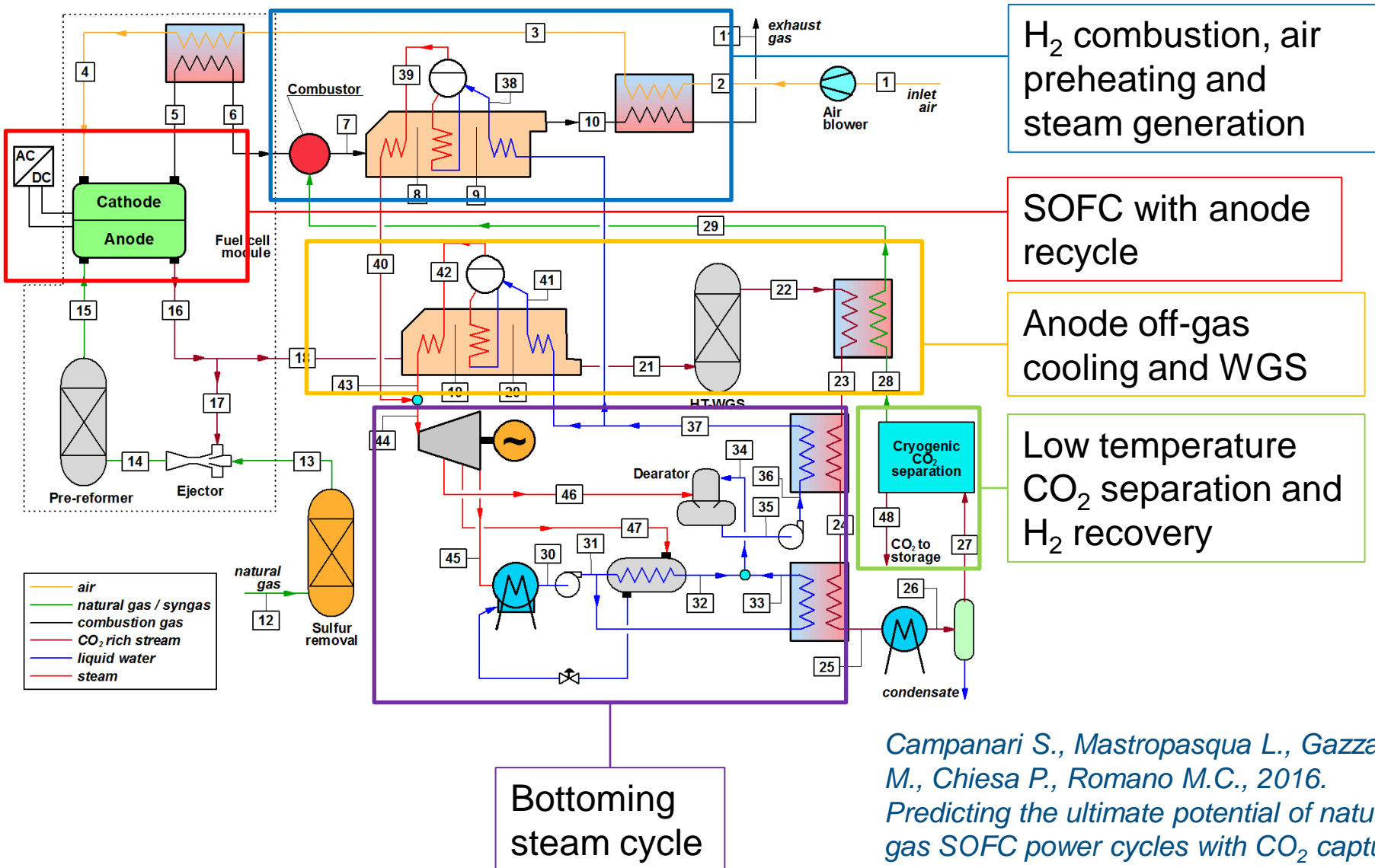
Syngas cooling and conditioning

H<sub>2</sub>-fired combined cycle

Adapted from:

Romano M.C., Chiesa P., Lozza G., 2010. Pre-combustion CO<sub>2</sub> capture from natural gas power plants, with ATR and MDEA processes; *Int J Greenh Gas Control*, 4, 785-797.

# Benchmark power plants – Low press. SOFC with CCS



H<sub>2</sub> combustion, air preheating and steam generation

SOFC with anode recycle

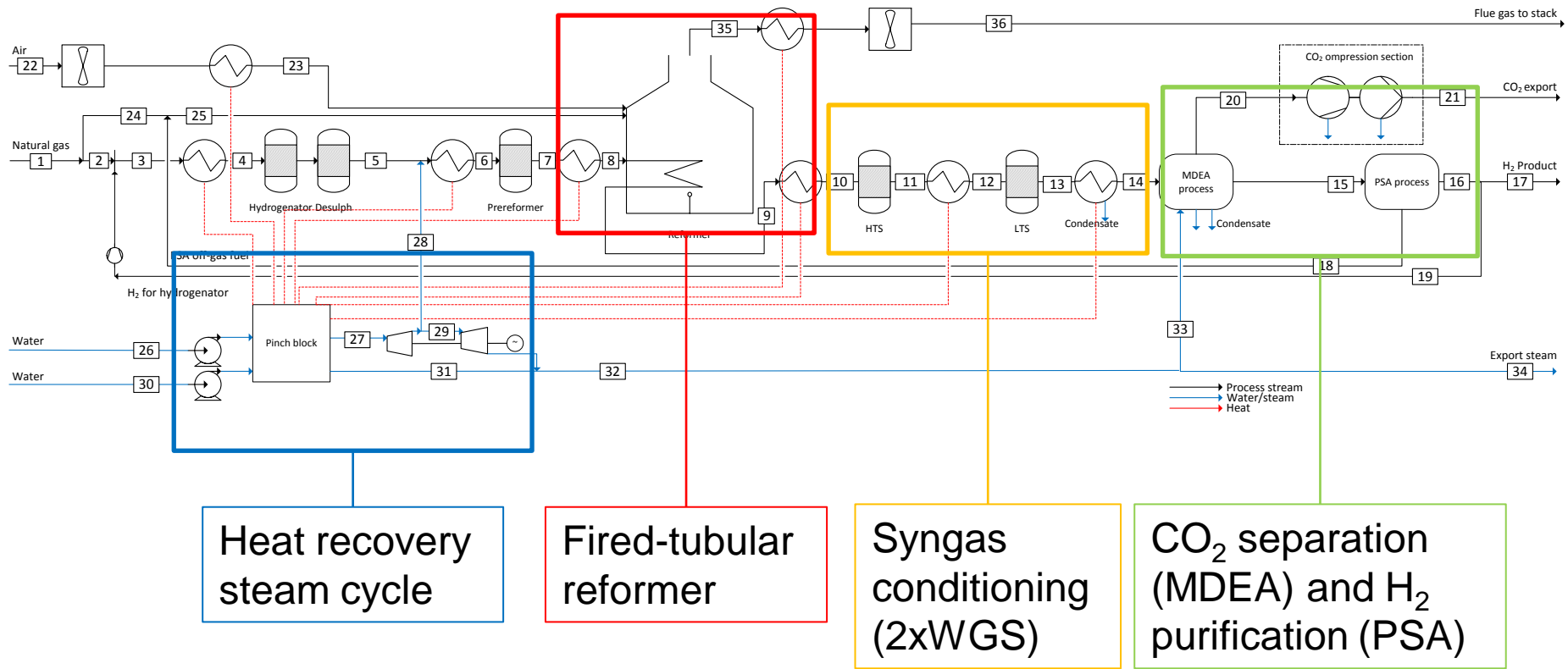
Anode off-gas cooling and WGS

Low temperature CO<sub>2</sub> separation and H<sub>2</sub> recovery

Bottoming steam cycle

Campanari S., Mastropasqua L., Gazzani M., Chiesa P., Romano M.C., 2016. Predicting the ultimate potential of natural gas SOFC power cycles with CO<sub>2</sub> capture; *Journal of Power Sources*, 324, 598-614. *Journal of Power Sources*, 325, 194-208.

# Benchmark hydrogen plants – FTR with CCS



Martínez I., Romano M.C., Fernández J.R., Chiesa P., Murillo R., Abanades J.C., 2014. Process design of a hydrogen production plant from natural gas with CO<sub>2</sub> capture based on a novel Ca/Cu chemical loop. *Applied Energy*, 114, 192-208.

Martínez I., Romano M.C., Chiesa P., Grasa G., Murillo R., 2013. Hydrogen production through sorption enhanced steam reforming of natural gas: thermodynamic plant assessment; *International Journal of Hydrogen Energy*, 38(35), 15180-15199.

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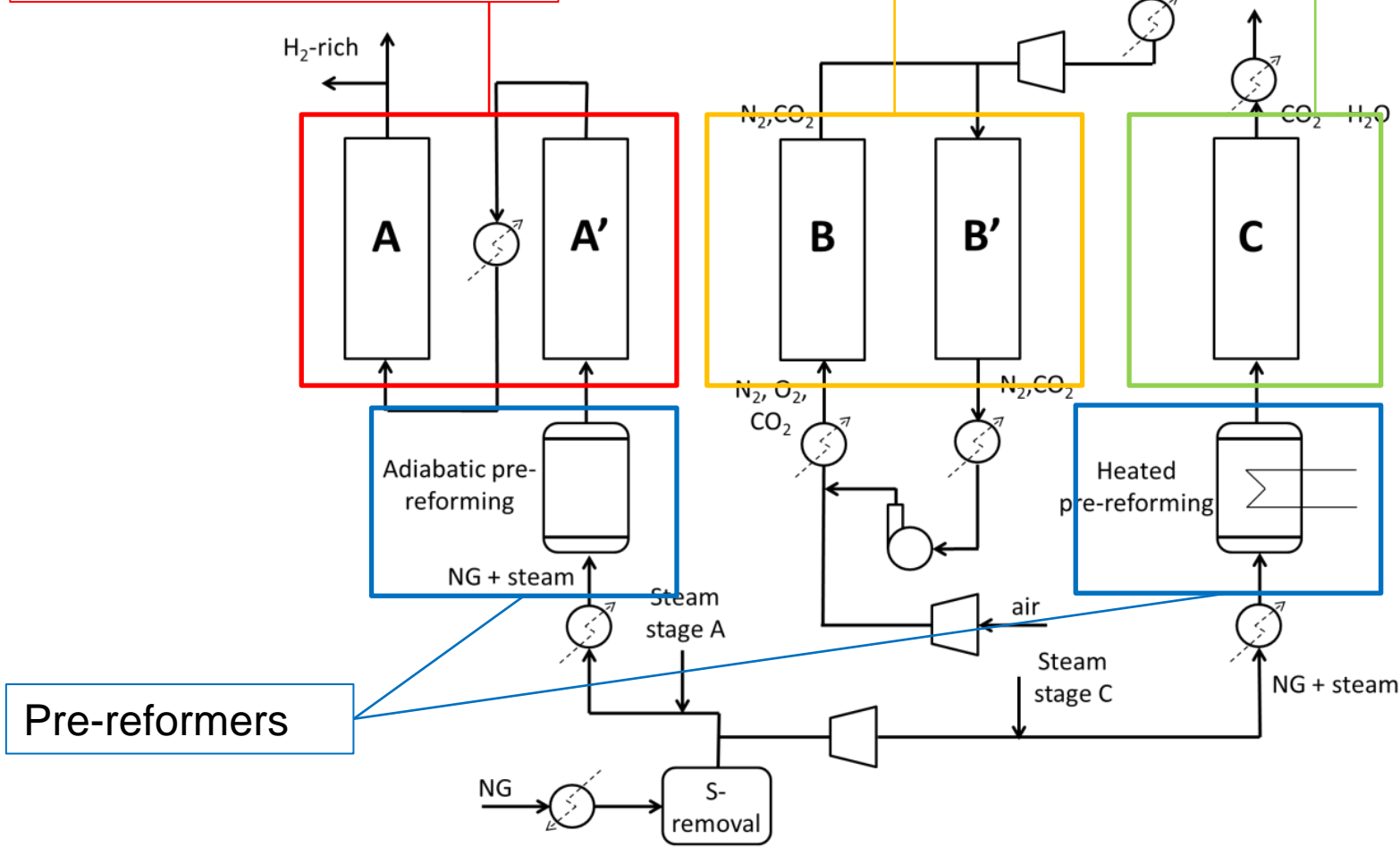


# Ca-Cu process for NGCC power plant

**Step A (~20 bar, S/C=5):**  
 $CH_4 + 2H_2O \rightarrow CO_2 + 4H_2$   
 $CaO + CO_2 \rightarrow CaCO_3$   
 (Cu)

**Step B (~20 bar):**  
 $Cu + 1/2O_2 \rightarrow CuO$   
 (CaCO<sub>3</sub>)

**Step C (1 bar):**  
 $4CuO + CH_4 \rightarrow CO_2 + 2H_2O$   
 $CaCO_3 \rightarrow CaO + CO_2$

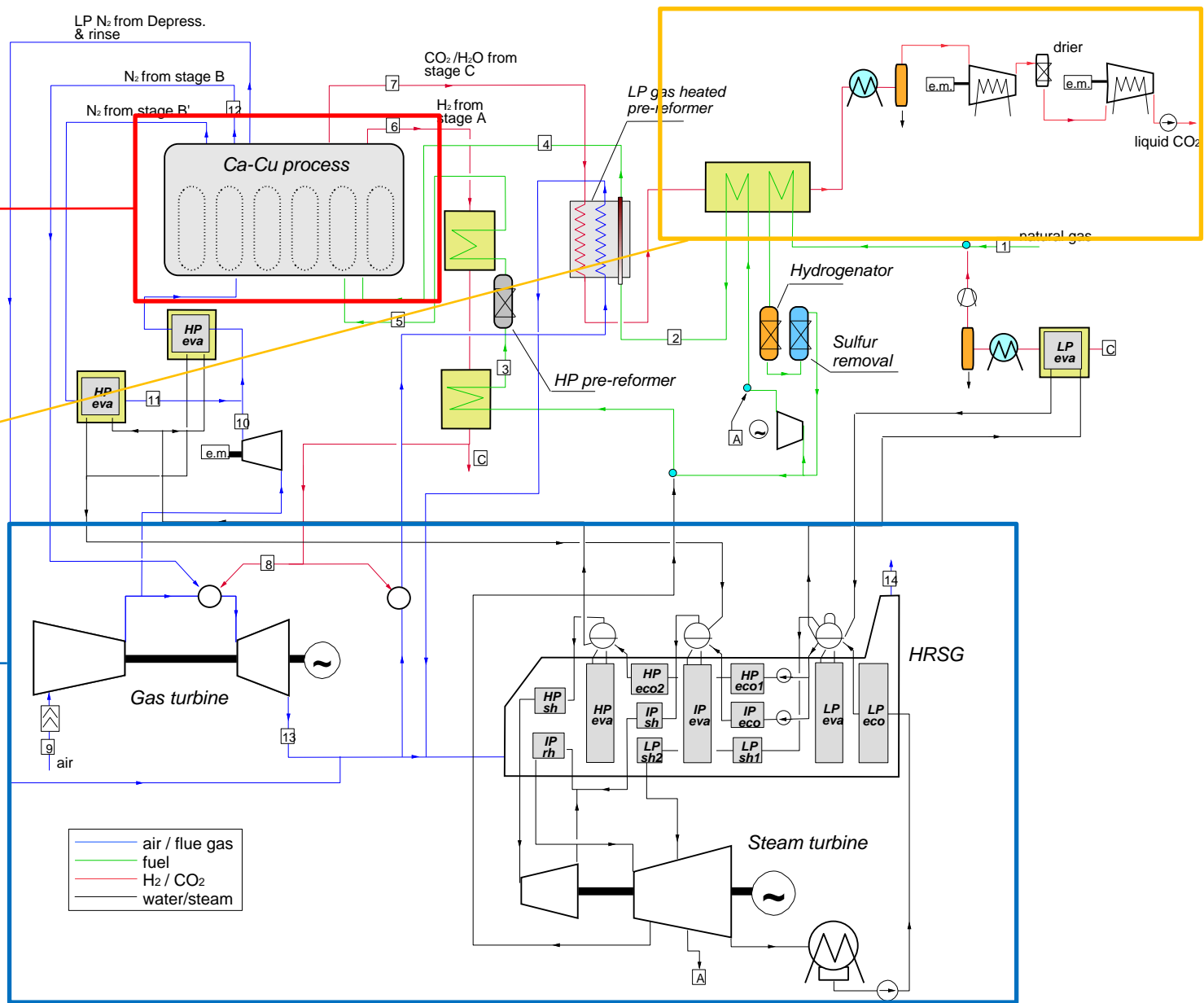


# Ca-Cu process for NGCC power plant

Ca-Cu process

CO<sub>2</sub> cooling and compression

H<sub>2</sub>-fired combined cycle



# SER for SOFC-based power plant

Bottoming steam cycle

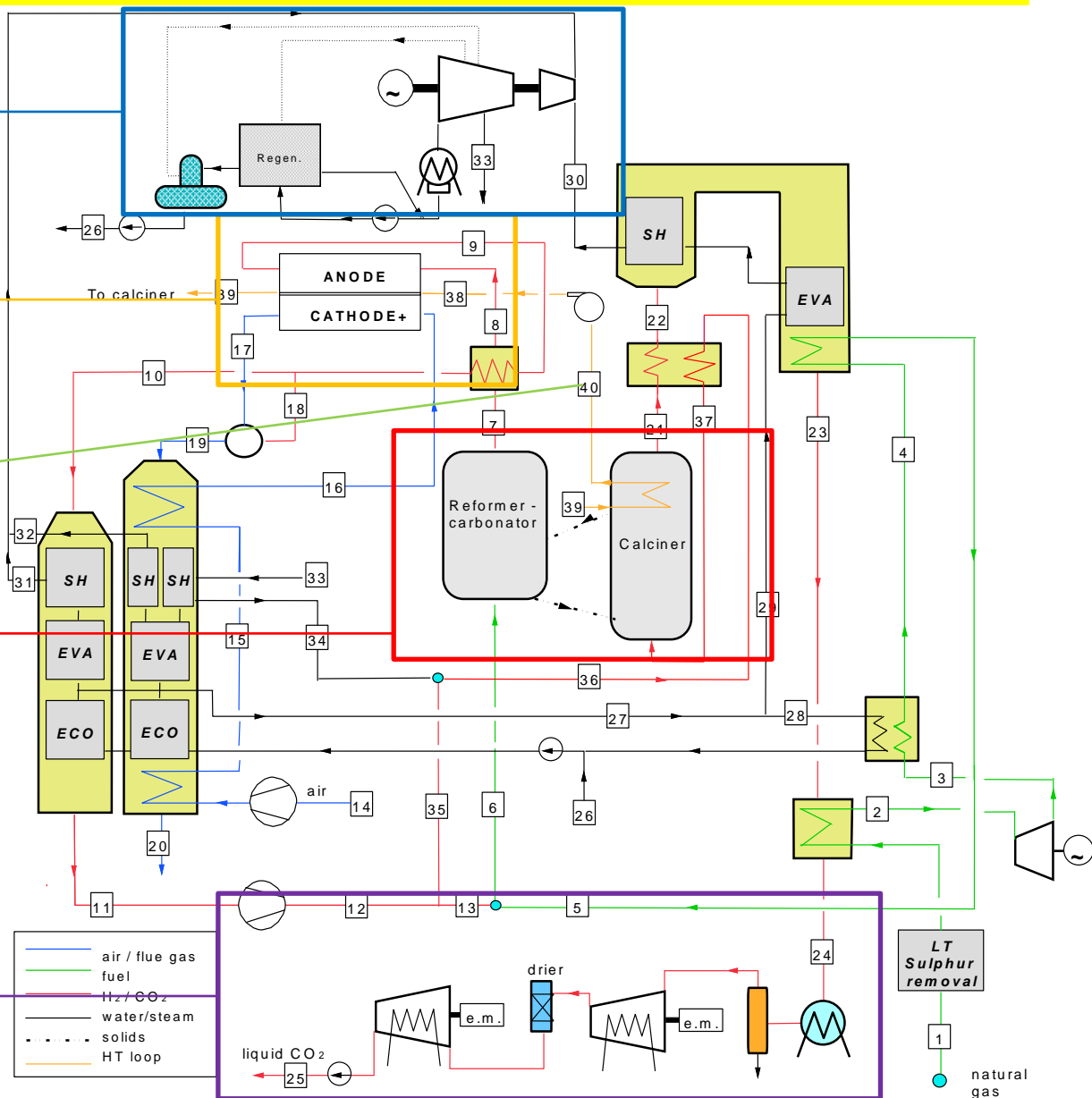
High temperature (~1000°C) SOFC

High temperature heat transfer loop

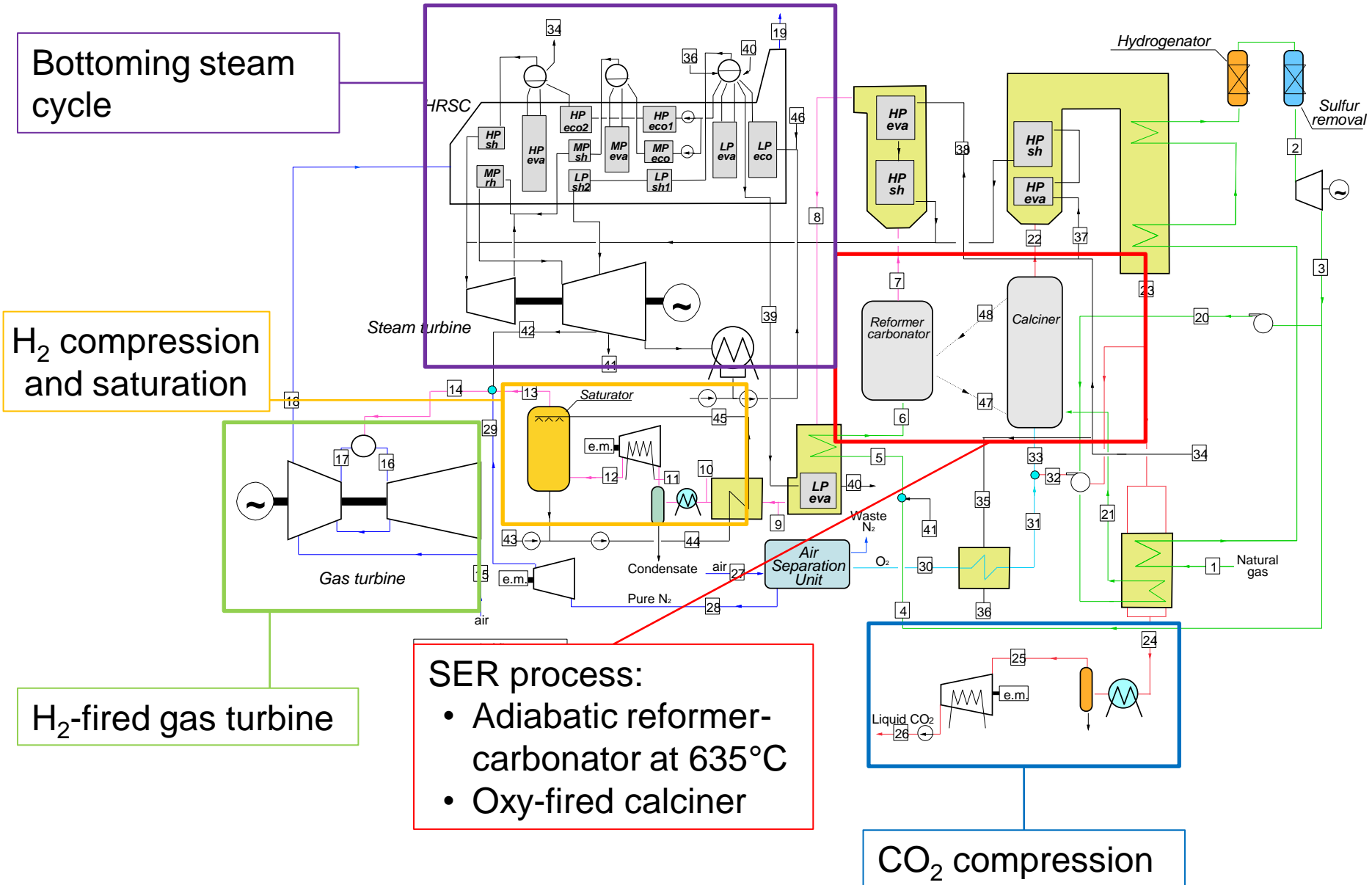
SER process:

- Adiabatic reformer-carbonator at 635°C
- Externally heated calciner at 865°C

CO<sub>2</sub> compression



# SER for NGCC-based power plants



# C-Shift process for NGCC power plant

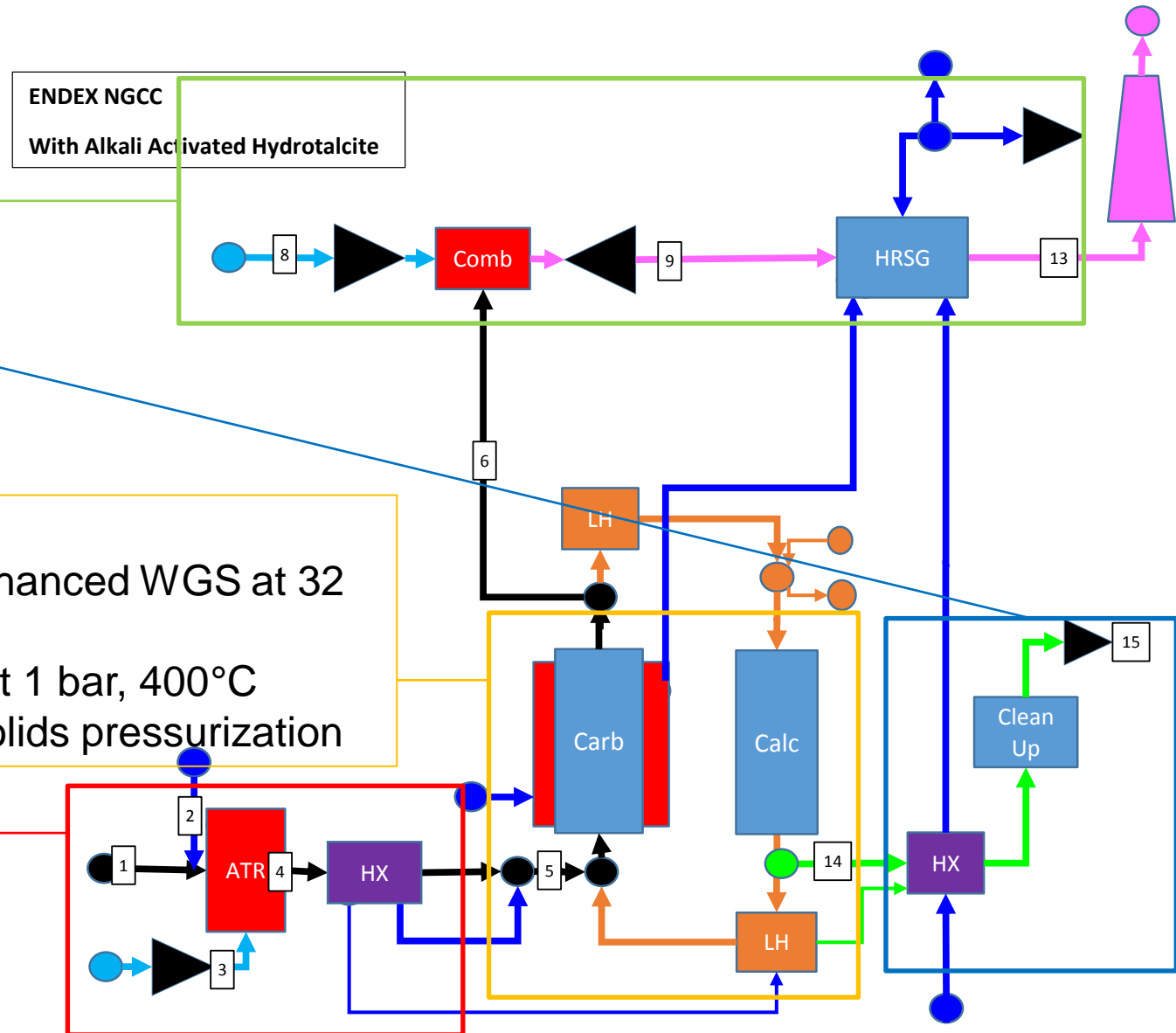
H<sub>2</sub>-fired combined cycle

CO<sub>2</sub> cooling and compression

C-Shift process:

- Cooled sorption-enhanced WGS at 32 bar, 440°C
- Adiabatic calciner at 1 bar, 400°C
- Lock-hoppers for solids pressurization

Air-blown ATR



## TRL of Ascent power plants

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A direct comparison and ranking of Ascent technologies is premature: the different power plants include technologies other than the Ascent ones with very different level of maturity.

# Low TRL components in Ascent power plants

| Ascent technology and component                          | Comments   |
|--|--|
| <b>All Ascent processes (except SER-SOFC plant)</b>      |  |
| H <sub>2</sub> -fired gas turbine                        | <p>No industrial application use hydrogen as GT fuel today. However, significant experimental tests on commercial GT machines have been performed with research purposes.</p> <p>→ under proper market conditions, commercial GTs may operate using hydrogen as fuel, after modifications of the combustor, the fuel system and possibly slightly modifying the firing temperature with respect to the corresponding NG-fired machine.</p> |
| <b>Ca-Cu process</b>                                     |  |
| No novel unit, too far from current industrial practice. |  |

# Low TRL components in Ascent power plants

| Ascent technology and component                                 | Comments  |
|---|---|
| <b>SER-SOFC process</b>   |   |
| Cooled SOFC   | No tests reported high temperature SOFC with external cooling circuit. Tests on externally cooled FC performed on PEM FC, operating at much lower temp..  |
| High temperature heat transfer loop and calciner heat exchanger | Lab-scale tests on the externally heated calciner performed at IFE. The heat transfer loop also includes high temperature piping and a high temperature fan. The operating temperature of these components is ~900°C, which is close to the temperature required in fired tubular reformer tubes. Duration tests to verify the resistance of such material at the specific conditions of the SER unit (high steam concentration, erosion by impacting solids, but low pressure differences) are needed. |
| <b>SER-NGCC process with externally heated calciner</b>         |   |
| High temperature heat transfer loop and calciner heat exchanger | Same considerations of the SER-SOFC system, except that no high temperature blower is needed, since gas pressure drops are balanced by GT compressor.   |
| <b>SER-NGCC process with oxyfuel calciner</b>                   |   |
| No novel unit, too far from current industrial practice.        | -   |



# Low TRL components in Ascent power plants

| Ascent technology and component | Comments   |
|---------------------------------|--|
| <b>C-Shift process</b>          |  |
| High temperature lock hoppers   | Lock hoppers are commercially available devices. However, operating conditions in the C-Shift process are more severe than in conventional applications, involving the pressurization and depressurization of solids at high temperatures. |

# Performance of Ascent CC power plants

|  | NGCC<br>w/o<br>capture | ATR +<br>MDEA | Ca-Cu<br>CC | Oxy-SER<br>CC | HE-SER CC                     | C-Shift<br>CC            |
|--|------------------------|---------------|-------------|---------------|-------------------------------|--------------------------|
| <b>Electric efficiency, %<sub>LHV</sub></b>      | 58.42                  | 47.12         | 47.78       | 46.3          | 46.1                          | 51.2                     |
| <b>Carbon capture ratio, %</b>                   |                        | 91.56         | 87.34       | 92.1          | 86.5                          | 88.3                     |
| <b>Specific emissions, kg/MWh</b>                | 350.6                  | 36.66         | 56.70       | 32.1          | 59.9                          | 46.9                     |
| <b>CO<sub>2</sub> avoided, %</b>                 |                        | 89.54         | 83.83       | 90.8          | 82.9                          | 86.6                     |
| <b>SPECCA, MJ<sub>LHV</sub>/kg<sub>CO2</sub></b> |                        | 4.71          | 4.67        | 5.04          | 5.67                          | 2.85                     |
| <b>Presence of additional low-TRL components</b> | -                      | -             | -           | -             | High temp. heat transfer loop | High. temp. lock hoppers |

Performance of Ca-Cu and oxy-SER cases is similar to benchmark ATR+MDEA plant.

Margins exist for improving Ca-Cu plant performance.

Advantages on the economic side are however possible for both processes.

Promising performance, much better than the benchmark, for the C-Shift process. More detailed modelling of the reactors is needed to confirm these performance.

# Performance of Ascent SOFC power plant

|  | Atmospheric SOFC w/o capture | Atmospheric SOFC with capt. | SER-SOFC   |
|--|------------------------------|-----------------------------|--|
| <b>Electric efficiency, %<sub>LHV</sub></b>      | 76.14                        | 72.48                       | <b>70.58</b>   |
| <b>Carbon capture ratio, %</b>                   | -                            | 84.87                       | <b>93.90</b>   |
| <b>Specific emissions, kg/MWh</b>                | 269.36                       | 42.66                       | <b>17.70</b>   |
| <b>CO<sub>2</sub> avoided, %</b>                 | -                            | 84.16                       | <b>93.43</b>   |
| <b>SPECCA, MJ<sub>LHV</sub>/kg<sub>CO2</sub></b> | -                            | 1.05                        | <b>1.48</b>  |
| <b>Presence of additional low-TRL components</b> | -                            | -                           | <b>Cooled SOFC &amp; high temp. heat transfer loop</b> |

Performance of SER-SOFC plant slightly worse than the SOFC-benchmark in terms of SPECCA. Performance improvement is possible if sorbent performance is improved.

Advantages on the economic side are anyway possible.

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## Economic analysis – first approach

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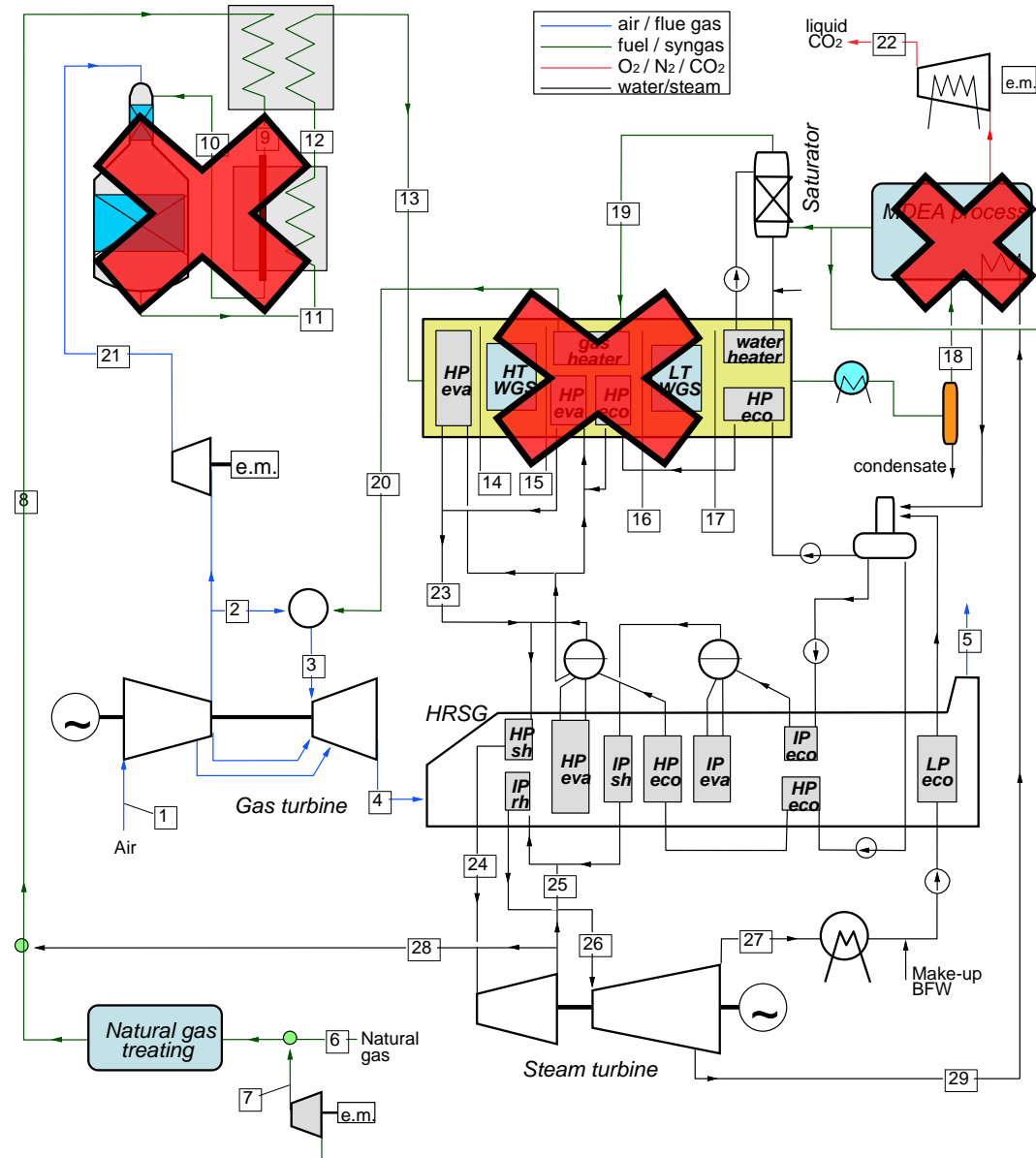
Due to the high uncertainty in estimating several components of novel Ascent processes, a differential economic analysis has been initially performed.

→ definition of an area of economic competitiveness for Capex and Opex of novel components/processes.

# Economic analysis – example of the CaCu plant

With respect to the benchmark ATR-NGCC power plant with CO<sub>2</sub> capture, CaCu plant features:

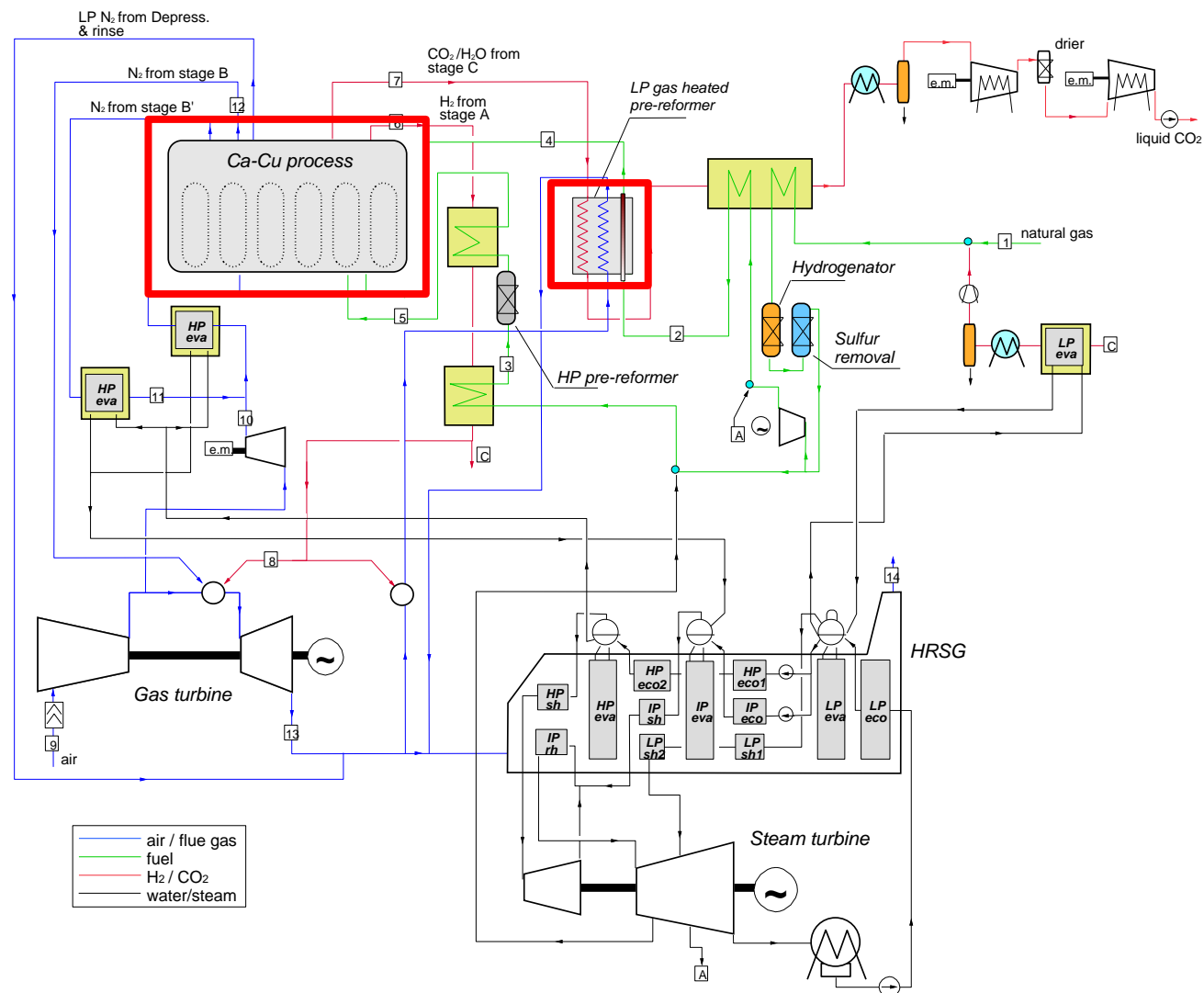
- No conventional reforming section → saving in Capex and opex for catalyst replacement
- No WGS reactors → saving in Capex and opex for catalyst replacement
- No CO<sub>2</sub> absorption process → saving in Capex and opex for solvent make-up
- Different size of steam cycle and cooling water system



# Economic analysis – CaCu plant

With respect to the benchmark ATR+NGCC power plant with CO<sub>2</sub> capture, CaCu plant features:

- CaCu chemical island → additional Capex and opex for catalyst, sorbent and oxygen carrier replacement
- LP gas heated pre-reformer → additional Capex and Opex



# Economic analysis – CaCu plant

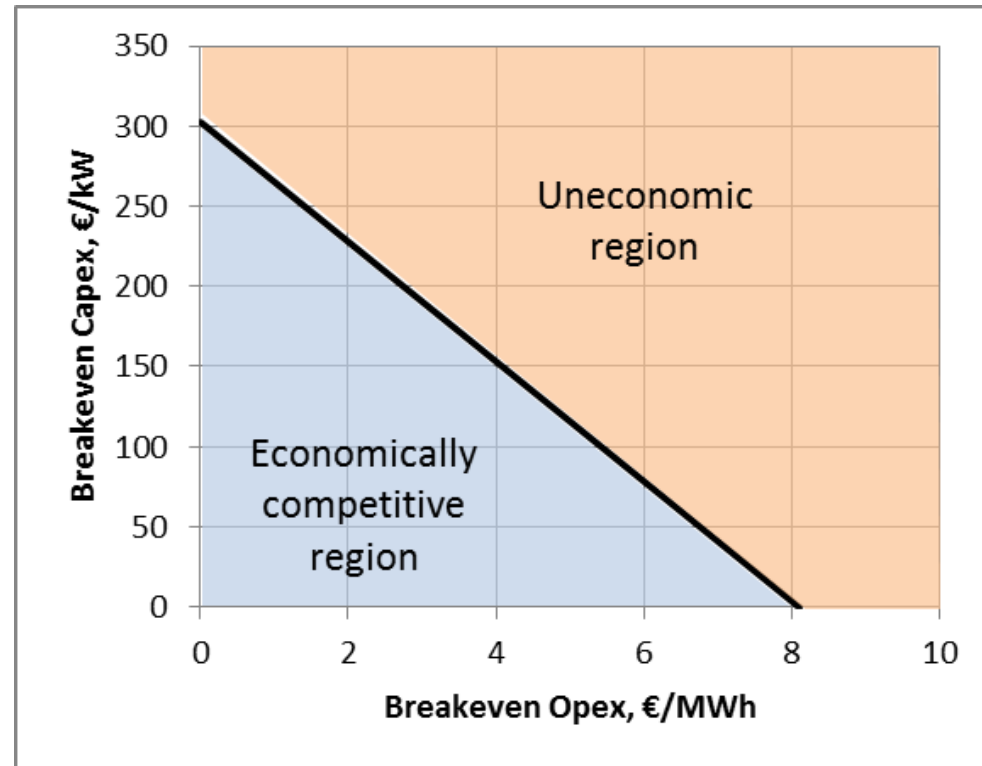
Cost of electricity and cost of CO<sub>2</sub> avoided:

|  | Benchmark<br>NGCC w/o<br>capture<br>€/MWh | Benchmark<br>ATR-NGCC<br>with capture<br>€/MWh | CaCu (zero<br>CaCu<br>cost)<br>€/MWh | CaCu<br>(breakeven<br>Capex)<br>€/MWh | CaCu<br>(breakeven<br>Opex)<br>€/MWh |
|--|---|--|--------------------------------------|---------------------------------------|--------------------------------------|
| Capital cost                                 | 11.72                                     | 25.48  | 19.38                                | <b>25.08</b>                          | 19.50                                |
| Natural gas                                  | 40.84                                     | 50.63  | 50.45                                | 50.45                                 | 50.45                                |
| Other variable O&M                           | 0.51                                      | 3.58   | 2.11                                 | 2.11                                  | <b>10.22</b>                         |
| Fixed O&M                                    | 5.45                                      | 10.90  | 8.28                                 | 10.82                                 | 8.28                                 |
| <b>Cost of Electricity</b>                   | <b>58.52</b>                              | <b>90.60</b>                                   | <b>80.22</b>                         | <b>88.45</b>                          | <b>88.45</b>                         |
| <b>Cost of CO<sub>2</sub> Avoided, €/ton</b> |   | <b>102.1</b>                                   | <b>74.0</b>                          | <b>102.1</b>                          | <b>102.1</b>                         |



# Economic analysis – CaCu plant

Maximum Capex and Opex of novel process units should be in the economically competitive region to make the technology competitive (from the point of view of the cost of CO<sub>2</sub> avoided).



Similar charts have been made for all the other plants, representing target economic performance for the technology developers.

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## Conclusions and next activities

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- Ca-Cu CC, oxy-SER CC and SER-SOFC power plants show efficiencies and SPECICA in line with the benchmark. Margin exists for improving the integrated processes. Economic benefits over benchmark technologies are possible.
- C-Shift power plants show efficiencies and SPECICA significantly better than the benchmark. Improved reactors modelling is needed to confirm this result. For this technology, the development of high temperature lock-hoppers is needed beyond Ascent.
- Work is ongoing to improve process performance of Ascent technologies in power plants and to include the effects of improved accuracy of the reactors models.
- Work is ongoing on process integration of Ascent technologies in hydrogen and ammonia production plants, with promising results.
- Work is ongoing to complete the economic analysis of Ascent power plants.

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Thank you

*The ASCENT project as part of the European Union's Seventh Framework Programme (FP7/2007-2013) under grant agreement n° 608512.*



[www.ascentproject.eu](http://www.ascentproject.eu)